

(a)

$$n_e = \frac{N_e}{V} = 2 \frac{(2\pi m_e kT)^{3/2}}{h^3} e^{-(E_g - E_F)/kT}$$

$$n_v = \frac{N_v}{V} = \dots \dots \dots e^{-E_F/kT}$$

$$n_e = n_v \Rightarrow E_F = \frac{E_g}{2}$$

$$n_e n_v = n_i^2 = \frac{4(2\pi m kT)^3}{h^6} e^{-E_g/kT}$$

$$n_e = \mu_e E \quad n_v = \mu_v E$$

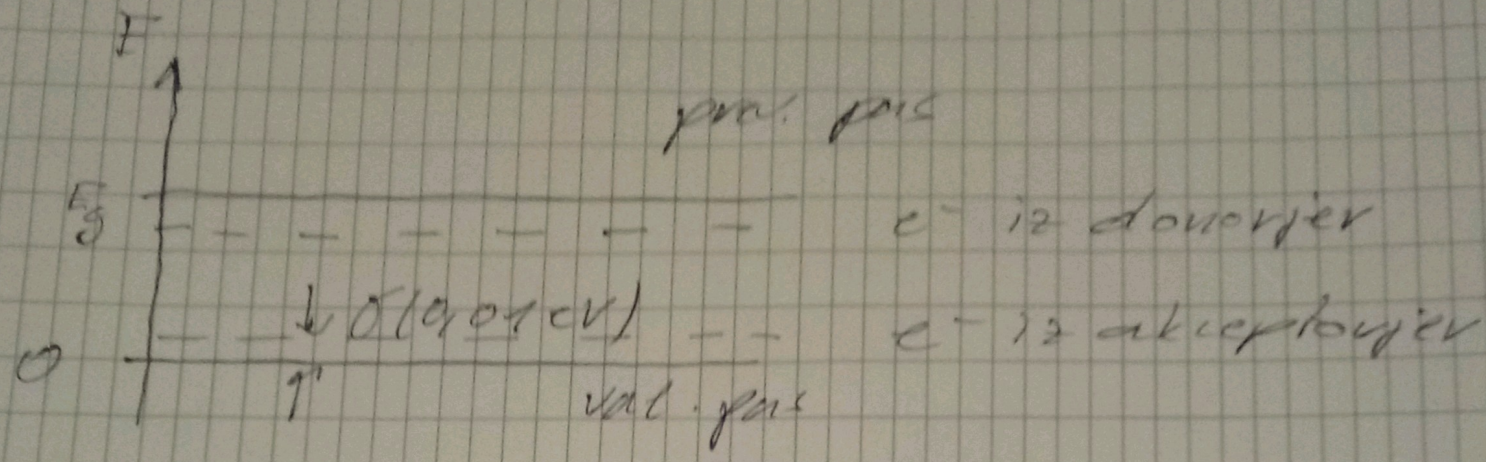
$$j = e_0 n_i (n_e + n_v) = e_0 n_i (\mu_e + \mu_v) E$$

$$m_e \neq m_v \Rightarrow$$

$$\mu = \frac{E_g}{2} - \frac{3}{4} kT \ln \frac{m_e}{m_v}$$

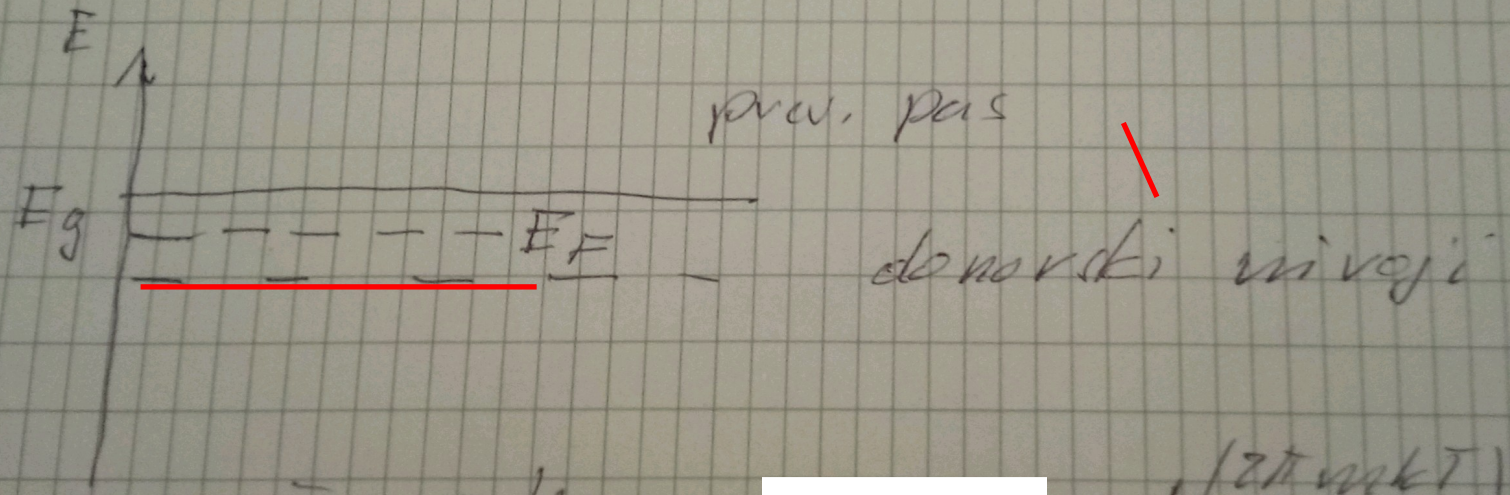
(b)

Dopirani polprevodniki



$E_g \sim 0.1 \text{ eV}$

tipični donorji: As, P, Li
 - II - akceptorji: B, Ga



se vedno

$n^2 =$

$= 4 \left(\frac{2\pi m k T}{h^2} \right)^3$

gostota prostih nosilcev naboja, ki izvirajo iz čistega polprev. - e^- iz valenčnega pasu in vrzeli iz prevodnega pasu

$e^{-E_g / kT}$

(ker $n_e n_v \neq f(E_F)$)

$$n_V + N_D = n_e + N_A$$

↓
gost. donorskih
atomov (+)

↓
gost. acceptorskih
atomov (-)

n-tip polprevodnika:

$$N_A = 0, N_D \neq 0$$

$$n_e \gg n_V$$

$$n_e \approx N_D$$

p-tip polprevodnika:

$$N_D = 0, N_A \neq 0$$

$$n_V \gg n_e$$

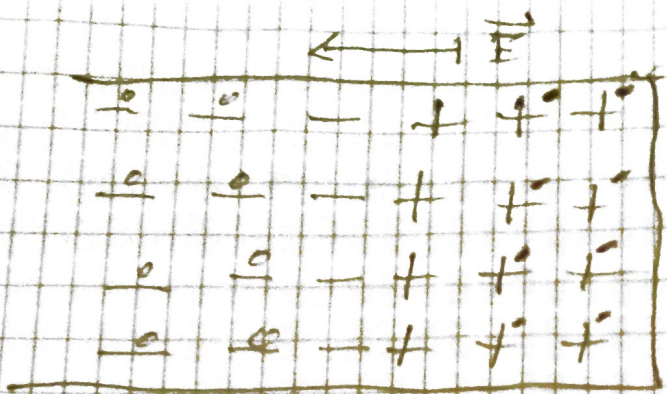
$$n_V \approx N_A$$

n-tip:

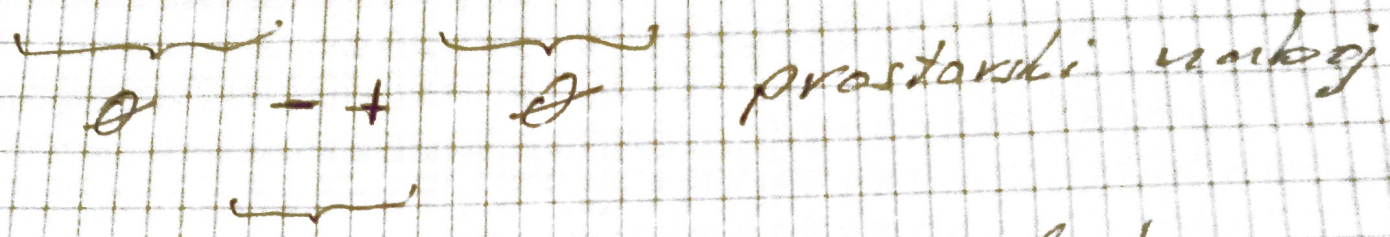
$$\sigma \approx e_0 N_D \mu_e$$

p-tip:

$$\sigma \approx e_0 N_A \mu_V$$



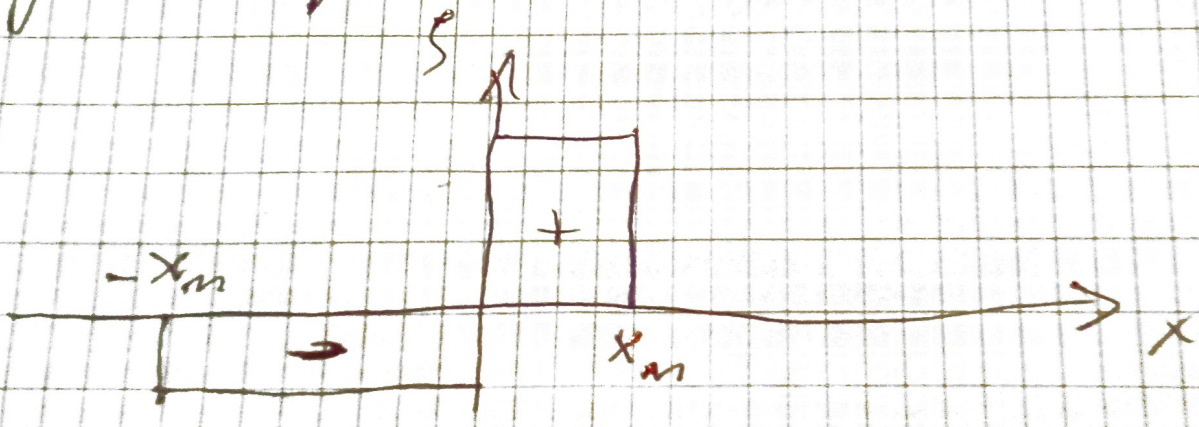
difuzija e- in
vrzeli je
samouklopien
proces



↳ depletivna plast

depletivna: brez gibljivih
nosilcev naboja (e- in
vrzeli)

gostota prostorskega naboja:



Maxwell-ova enačba:

$$\vec{\nabla} \cdot \vec{E} = \frac{\rho(\vec{r})}{\epsilon \epsilon_0}$$

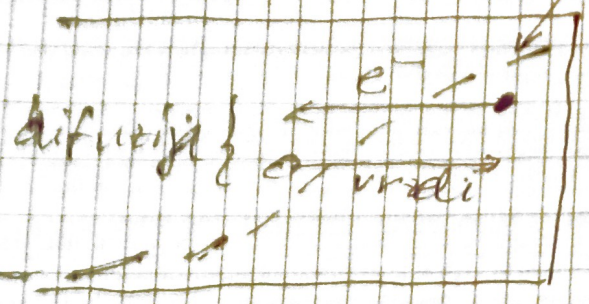
(d)

p-tip
pri mesji akceptorja

p-tip

← kompenzacija
← Li (donor)

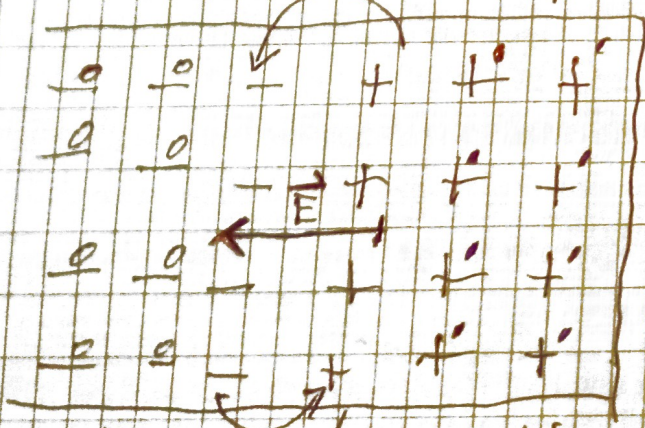
gostota Li
atomov



visja
gostota
vzeli (vzeli
akceptorskih atomov)

visja gostota e- (vzeli
donorskih atomov)

e- oddifundirajo



p-tip vzeli
oddifund. n-tip

- + : donorski ion
- : akceptorski ion
- +^o : donorski atom
- ^o : akceptorski atom

(f)

02. v 1D:

$$\frac{\partial E}{\partial x} = \frac{\rho(x)}{\epsilon \epsilon_0}$$

→ potencial

$$\vec{E} = -\vec{\nabla} V$$
$$E = -\frac{\partial V}{\partial x}$$

→ $\frac{\partial^2 V}{\partial x^2} = -\frac{\rho(x)}{\epsilon_0}$ Poissonova lu.

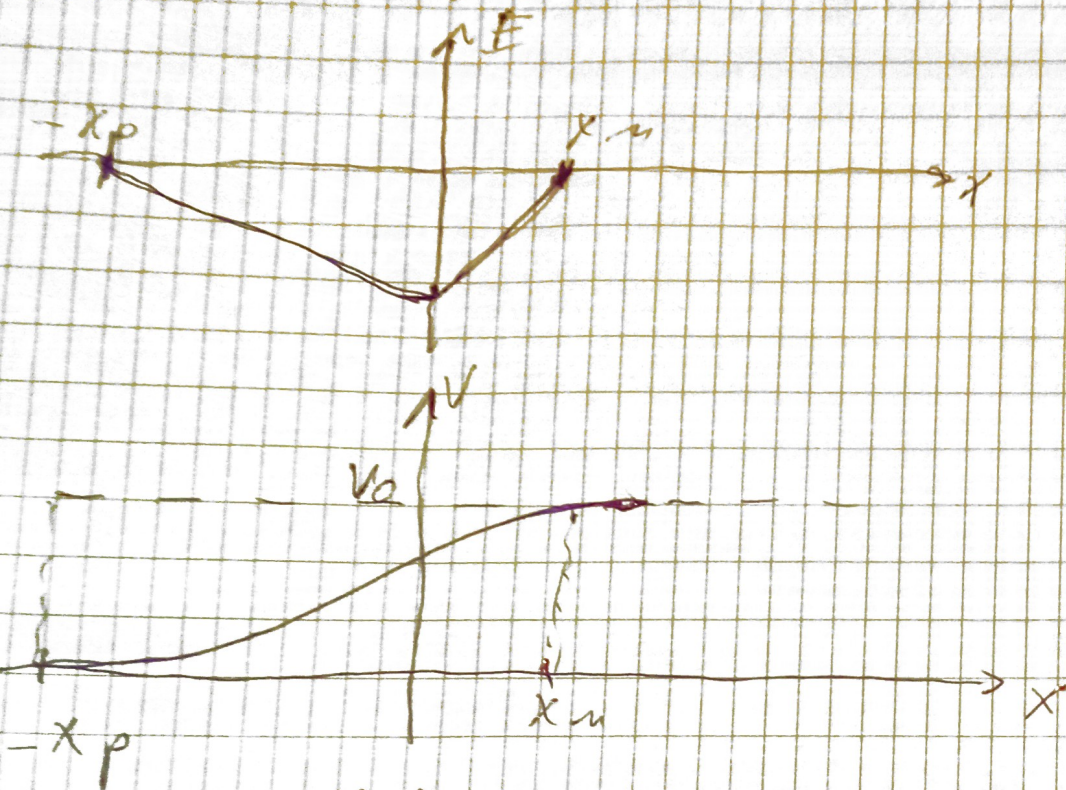
$$\rho(x) = \begin{cases} eN_D & 0 \leq x \leq x_n \\ -eN_A & -x_p \leq x \leq 0 \end{cases}$$

$$E = -\frac{\partial V}{\partial x} = \begin{cases} \frac{eN_D}{\epsilon \epsilon_0} (x - x_n) & 0 \leq x \leq x_n \\ -\frac{eN_A}{\epsilon \epsilon_0} (x + x_p) & -x_p \leq x \leq 0 \end{cases}$$

(robní pogoji: $E = 0$ za $x = x_n, -x_p$)

$$V(x) = \begin{cases} -\frac{eN_D}{2\epsilon\epsilon_0} (x-x_m)^2 + V_0 & 0 < x \leq x_m \\ \frac{eN_A}{2\epsilon\epsilon_0} (x+x_p)^2 & -x_p \leq x < 0 \end{cases} \quad (2)$$

(ročni pogoji: $V(x_m) = V_0$, $V(-x_p) = 0$)



$V(x)$ zvečan pri $x=0 \Rightarrow$

$$\Rightarrow V_0 = \frac{e}{2\epsilon\epsilon_0} (N_D x_m^2 + N_A x_p^2)$$

po tej tega je snov nevtralen elek.

neutralen $\Rightarrow Q_+ = Q_- \Rightarrow$

$$\Rightarrow N_A x_p = N_D x_m$$

(4)

$$\Rightarrow x_n = \left[\frac{2 \epsilon \epsilon_0 V_0}{e N_D (1 + N_D / N_A)} \right]^{1/2}$$

$$x_p = \left[\frac{2 \epsilon \epsilon_0 V_0}{e N_A (1 + N_A / N_D)} \right]^{1/2}$$

celotna debelina depletirane plasti:

$$d = x_n + x_p = \left[\frac{2 \epsilon \epsilon_0 V_0}{e} \frac{N_A + N_D}{N_A N_D} \right]^{1/2}$$

p stran močnejše dopirana kot n stran

$$N_A \gg N_D \Rightarrow x_n \gg x_p \Rightarrow$$

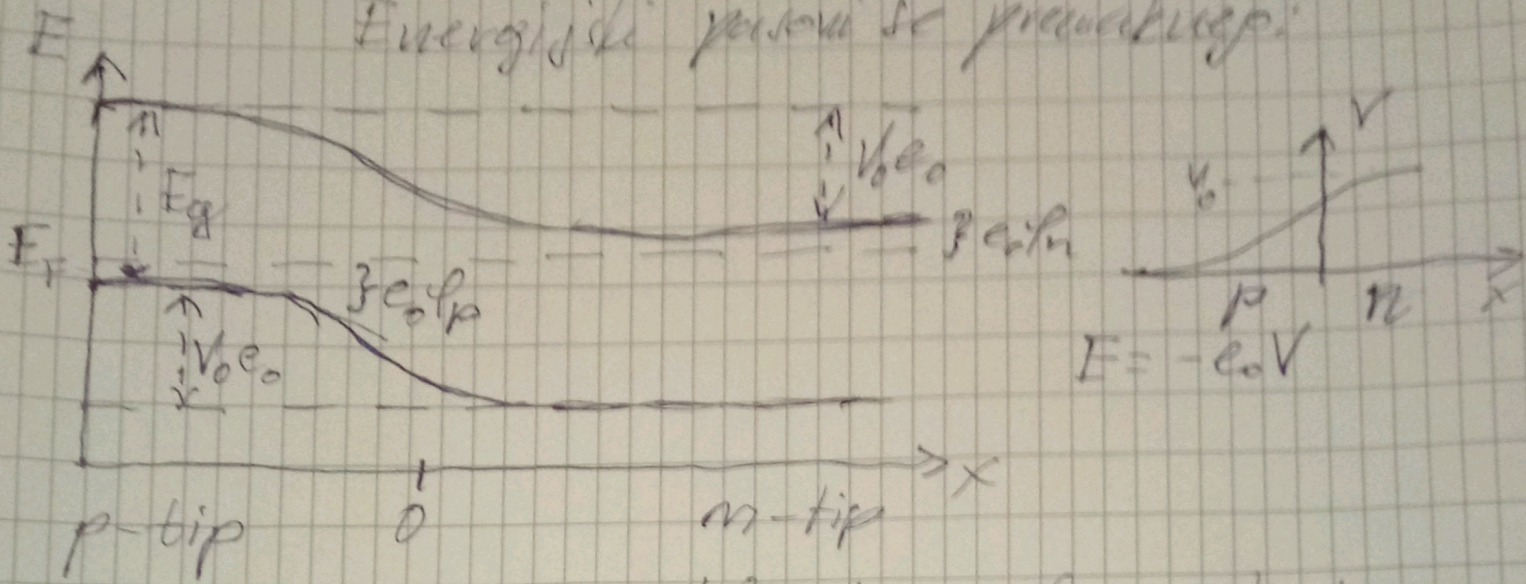
$$\Rightarrow d \approx x_p$$

in obratno...

(1)

Kaj pomena kontaktne napetosti V_0 za e^- ?

Energijski pasovi se preoblikujejo:



e^- (rečinski gibljivi nosilci naboga v n-tipu) morajo premagati potencialni skok, da preidejo iz n strani na p.

Čist polprev.: $n_e = n_0 e^{-(E_g - E_F)/kT}$
 $n_v = n_0 e^{-E_F/kT}$

Dopiran polprev.:

$n_e = n_0 e^{-e_0 \psi_0 / kT}$
 $n_v = n_0 e^{-e_0 \psi_0 / kT}$

$$F_F + e_0 \psi_n + e_0 \psi_p - F_g + e_0 \psi_n = F_F$$

$$V_0 = \frac{F_g}{e_0} = (\psi_n + \psi_p)$$

$$\psi_{n,p} = \frac{kT}{e_0} \ln \frac{n_0}{n_0, p}$$

$$V_0 = \frac{F_g}{e_0} - \frac{kT}{e_0} \ln \frac{n_0^2}{n_0, e n_0, v}$$

$$n_0^2 = n_0^2 e^{-F_g/kT} \rightarrow n_0^2 = n_0^2 e^{F_g/kT}$$

$$V_0 = \frac{kT}{e_0} \ln \frac{n_0, e n_0, v}{n_0^2}$$

$$n_0, e \approx N_D \quad n_0, v = N_A$$

$$V_0 = \frac{kT}{e_0} \ln \frac{N_D N_A}{n_0^2}$$

$$N_{D,A} \sim 10^{17} / \text{cm}^3$$

$$N_{at} \sim 10^{22} / \text{cm}^3$$

$$n_0 \sim 10^{10} / \text{cm}^3$$

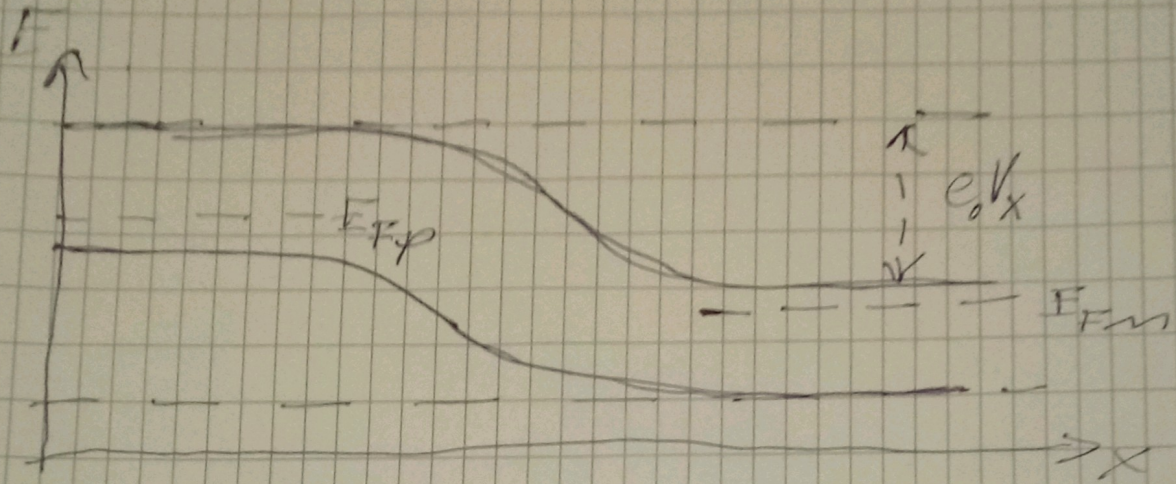
$$T = 300 \text{ K}, N_A = N_D = 10^{17} / \text{cm}^3 \Rightarrow$$

$$\Rightarrow V_0^{Si} \approx 0,9 \text{ V}$$

(2)

$$V_0 \sim 0,2V \rightarrow d \sim 50 \mu m$$

Če dodamo zunanjo zaporno napetost (+ na le strani, - na pr strani):



$$E_{Fp} - E_{Fn} = e_0 V_b$$

$$E_{Fn} + e_0 \psi_n + e_0 V_x - E_g + e_0 \psi_p = E_{Fp}$$

$$e_0 V_x = \underbrace{E_{Fp} - E_{Fn}}_{e_0 V_b} + \underbrace{E_g - e_0 \psi_n - e_0 \psi_p}_{e_0 V_0}$$

$$\Rightarrow V_x = V_b + V_0$$

brez V_b : da $\sqrt{V_0}$ z V_b : da $\sqrt{V_b + V_0} \approx \sqrt{V_0}$

Polprvodniška dioda

(2)

